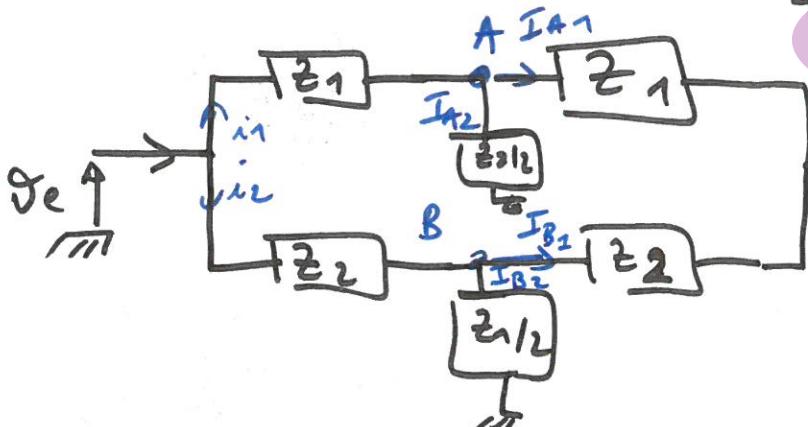


Exo 5 Double T en port .



⇒ recherche $\frac{V_x}{V_e}$ = fact de transfert

V_s tension à vide

$$\left. \begin{array}{l} * V_e - z_1 i_1 = V_A \\ V_A - \frac{z_2}{2} I_{A2} = 0 \\ V_A - z_1 I_{A1} = V_S \end{array} \right\} \quad \begin{array}{l} I_1 = I_{A2} + I_{A1} \\ \Rightarrow \frac{V_e - V_A}{z_1} = 2 \frac{V_A}{z_2} + \frac{V_A - V_S}{z_1} \end{array}$$

$$\Rightarrow V_e - V_A = 2 V_A \frac{z_1}{z_2} + V_A - V_S$$

$$\Rightarrow V_e + V_S = 2 V_A \left(\frac{z_1}{z_2} + 1 \right) = 2 V_A \frac{z_1 + z_2}{z_2}$$

$$\Rightarrow V_A = \frac{V_e + V_S}{2} \frac{z_2}{z_1 + z_2} \quad \textcircled{A}$$

par symétrie $A \rightarrow B$
 $z_1 \rightarrow z_2$

$$V_B = \frac{V_e + V_S}{2} \frac{z_1}{z_1 + z_2} \quad \textcircled{B}$$

$$* \underline{I_{A1} + I_{B1} = 0} \quad \text{fil non relié}$$

$$\frac{V_A - V_S}{z_1} + \frac{V_B - V_S}{z_2} = 0 \Rightarrow \frac{V_A}{z_1} + \frac{V_B}{z_2} = V_S \frac{z_1 + z_2}{z_1 z_2}$$

$$\Rightarrow V_S = \frac{z_1 z_2}{z_1 + z_2} \left[\frac{V_A}{z_1} + \frac{V_B}{z_2} \right] = \textcircled{V_A} \frac{z_2}{z_1 + z_2} + \textcircled{V_B} \frac{z_1}{z_1 + z_2}$$

$$\Rightarrow V_S = \left(\frac{z_2}{z_1 + z_2} \right)^2 \frac{V_e + V_S}{2} + \left(\frac{z_1}{z_1 + z_2} \right)^2 \frac{V_e + V_S}{2}$$

$$V_S = \frac{V_e + V_S}{2} \left[\frac{z_2^2 + z_1^2}{(z_1 + z_2)^2} \right] \Rightarrow \frac{V_e + V_S}{2 V_S} = 2 \frac{(z_1 + z_2)^2}{z_1^2 + z_2^2}$$

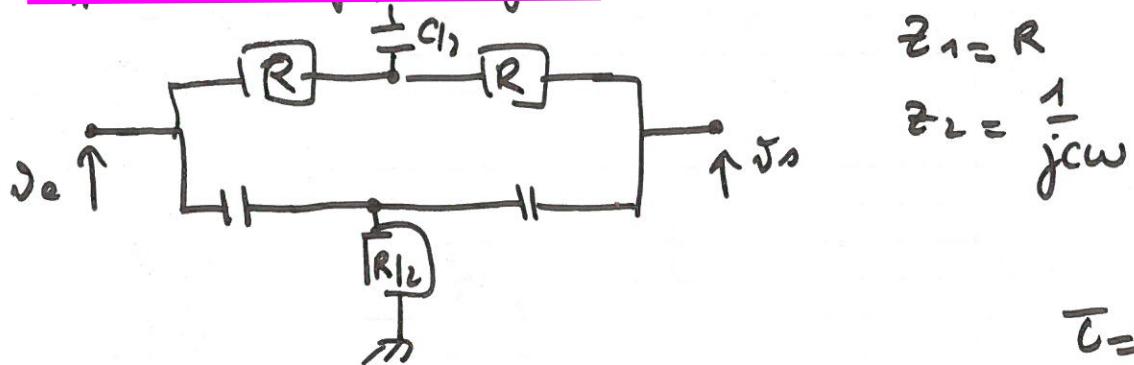
$$\frac{V_o}{V_e} + 1 = 2 \frac{(z_1 + z_2)^2}{z_1^2 + z_2^2} \Rightarrow \frac{V_o}{V_e} = \frac{2(z_1 + z_2)^2}{z_1^2 + z_2^2} - 1$$

$$\frac{V_o}{V_e} = \frac{2z_1^2 + 2z_2^2 + 4z_1z_2 - z_1^2 - z_2^2}{z_1^2 + z_2^2} = \frac{(z_1 + z_2)^2 + 2z_1z_2}{z_1^2 + z_2^2}$$

$$= \frac{z_1^2 + z_2^2 + 4z_1z_2}{z_1^2 + z_2^2}$$

$$\frac{V_o}{V_e} = \frac{(z_1^2 + z_2^2)}{z_1^2 + z_2^2 + 4z_1z_2} = \frac{1}{1 + 4 \frac{z_1z_2}{z_1^2 + z_2^2}} \quad \text{fct de transfert}$$

application au filtre rejecteur



$$z_1 = R$$

$$z_2 = \frac{1}{j\omega C}$$

$$\tau = RC$$

$$\frac{V_o}{V_e} = \frac{1}{1 + 4 \frac{R/j\omega C}{R^2 - 1/C^2 \omega^2}} = \frac{1}{1 + \frac{4RC\omega}{j\omega^2 R^2 - j\omega^2 C^2}}$$

$$\frac{V_o}{V_e} = \frac{1}{1 + \frac{4\tau\omega}{j[\tau^2\omega^2 - 1]}} = \frac{1}{1 + \frac{4j\tau\omega}{\tau^2\omega^2 - 1}} = \frac{\tau^2\omega^2 - 1}{\tau^2\omega^2 - 1 - 4j\tau\omega}$$

$$\left| \frac{V_o}{V_e} \right| = \frac{|1 - \tau^2\omega^2|}{\sqrt{(\tau^2\omega^2 - 1)^2 + 16\tau^2\omega^2}}$$

Car pour étudier cette fct il faut en prendre le module.

$$\text{qd } \omega \rightarrow 0 \quad \left| \frac{V_o}{V_e} \right| \rightarrow 1$$

$$\text{qd } \omega \rightarrow +\infty \quad \left| \frac{V_o}{V_e} \right| \rightarrow 1 \quad \left(\frac{\frac{1}{1-4j\tau\omega}}{\tau^2\omega^2-1} \right) \quad \begin{cases} \text{filtre passe} \\ \text{haute} \\ \text{rejectant de la} \\ \text{pulse} \end{cases}$$

$$\omega \rightarrow 1/\tau \quad \left| \frac{V_o}{V_e} \right| \rightarrow 0$$

fréquence de coupure

$$\left| \frac{V_o}{V_e} \right|_{\omega=\omega_c} = \frac{\text{max}}{\sqrt{2}} \left| \frac{V_o}{V_e} \right| = 1/\sqrt{2}$$

$$\left| \frac{V_o}{V_e} \right|^2 = \frac{1}{2} = \frac{(1-\tau^2\omega_c^2)}{(1-\tau^2\omega_c^2)^2 + 16\tau^2\omega_c^2}$$

$$2(1-\tau^2\omega_c^2)^2 = (1-\tau^2\omega_c^2)^2 + 16\tau^2\omega_c^2$$

$$(1-\tau^2\omega_c^2)^2 = 16\tau^2\omega_c^2 \Rightarrow 1-\tau^2\omega_c^2 = \pm 4\tau\omega_c$$

$$\tau^2\omega_c^2 \neq 4\tau\omega_c + 1 = 0 \quad \Delta = 16\tau^2 + 4\tau^2 = 20\tau^2$$

$$\omega_{c1,2} = \frac{\mp 4\tau \pm 2\tau\sqrt{5}}{2\tau^2} \quad \text{fréq > 0} \text{ pas 1 seule solut}$$

$$\omega_{c1,2} = \pm \frac{1}{\tau} + \frac{1}{\tau}\sqrt{5} = \frac{2}{\tau} \left[\frac{\sqrt{5}}{2} \mp 1 \right]$$

$$\omega_{c1,2} = \frac{0.236/2}{4,236/2}$$

$$\Delta\omega = 4/\tau.$$

